

MICROFABRICATED ACOUSTIC TRANSDUCER WITH SUPPRESSED SUBSTRATE MODES

BACKGROUND OF THE INVENTION

Field of the Invention

The present invention relates to the field of acoustic transducers. More specifically, the present invention relates to capacitive microfabricated ultrasonic transducers.

Cross-Reference to Related Applications

This invention claims priority based on U.S. Provisional Application No. 60/242,298 filed October 19, 2001, entitled "Microfabricated Ultrasonic Transducer with Suppressed Substrate Modes."

Description of the Related Art

An acoustic transducer is an electronic device used to emit and receive sound waves. Acoustic transducers are used in medical imaging, non-destructive evaluation, and other applications. Ultrasonic transducers are acoustic transducers that operate at higher frequencies. Ultrasonic transducers typically operate at frequencies exceeding 20 kHz.

The most common forms of ultrasonic transducers are piezoelectric transducers. Recently, a different type of ultrasonic transducer, capacitive microfabricated transducers, have been described and fabricated. Such transducers are described by Haller et al. in U.S. Patent No. 5,619,476 entitled "Electrostatic Ultrasonic Transducer," issued April 9, 1997, and Ladabaum et al. in U.S. Patent No. 5,870,351 entitled "Broadband Microfabricated Ultrasonic Transducer and Method of Fabrication," issued February 9, 1999. These patents describe transducers capable of functioning in a gaseous environment, such as air-coupled transducers. Ladabaum et al, in U.S. Patent No. 5,894,452 entitled, "Microfabricated Ultrasonic Immersion Transducer," issued April 13, 1999 describe an immersion transducer (a transducer capable of operating in contact with a liquid medium), and in U.S. Patent No. 5,982,709 entitled, "Acoustic Transducer and Method of Microfabrication," issued November 9, 1999 describe improved structures and methods of microfabricating immersion transducers. The basic transduction element described by these patents is a vibrating capacitor. A substrate contains a lower electrode, a thin diaphragm is suspended over said substrate, and a metalization layer serves as an upper electrode. If a DC

1 bias is applied across the lower and upper electrodes, an acoustic wave impinging on the
2 diaphragm will set it in motion, and the variation of electrode separation caused by such motion
3 results in an electrical signal. Conversely, if an AC signal is applied across the biased electrodes,
4 an AC forcing function will set the diaphragm in motion, and this motion emits an acoustic wave
5 in the medium of interest.

6 It has been realized by the present inventors that the force on the lower (substrate)
7 electrode cannot be ignored. Even though the diaphragm is much more compliant than the
8 substrate and thus moves much more than the substrate when an AC voltage is applied between
9 the biased electrodes, the substrate electrode experiences the same electrical force as the
10 diaphragm electrode. Thus, when transmitting, a microfabricated ultrasonic transducer can
11 launch acoustic waves in the substrate as well as in the medium of interest, even though the
12 particle motion in the substrate is smaller than the particle motion in the fluid medium of interest.
13 Of particular concern is the situation where the substrate has mechanical properties and a
14 geometry such that resonant modes can be excited by the force on the substrate electrode. In
15 these cases, the acoustic activity of the substrate can undermine the performance of the
16 transducer. One specific example is a longitudinal ringing mode that can be excited in a typical
17 silicon substrate wafer. Since the detrimental effects on transducer performance of the forces
18 and motion of the substrate electrode have not been previously addressed, there is the need for an
19 ultrasonic transducer capable of operating with suppressed substrate modes.

20 While the suppression of modes, matching, and the damping of acoustic energy exists in
21 piezoelectric transducers, the differences between such piezoelectric transducers and
22 microfabricated ultrasonic transducers are so numerous that heretofore suppression of modes,
23 matching and damping was not considered relevant to microfabricated ultrasonic transducers.
24

25 SUMMARY OF THE INVENTION

26 It is an object of the present invention to provide microfabricated acoustic or ultrasonic
27 transducer with suppressed substrate acoustic modes.

28 It is a further object of the present invention to provide an acoustic or ultrasonic
29 transducer with suppressed substrate acoustic modes when the substrate is a silicon wafer
30 containing integrated electronic circuits.

1 It is a further object of the present invention to provide an acoustic damping material
2 placed on the back side of the substrate, said backing material capable of dissipating the acoustic
3 energy in the substrate.

4 It is a further object of the present invention to provide a thinned substrate so that
5 acoustic modes in the substrate can exist only at frequencies outside the band of interest.

6 It is a further object of the present invention to provide a specific material capable of
7 suppressing modes in a silicon substrate.

8 The present invention achieves the above objects, among others, with an acoustic or
9 ultrasonic transducer comprised of a diaphragm containing an upper electrode suspended above a
10 substrate containing the lower electrode, a substrate that may or may not contain electronic
11 circuits, and a backing material that absorbs acoustic energy from the substrate. Further, the
12 substrate can be thinned to dimensions such that, even without any backing material, resonant
13 modes are outside of the frequency band of interest.

14 In order to obtain a suitable backing material to dampen the acoustic energy in the
15 substrate is twofold, certain characteristics are preferably met. First, the material should have an
16 acoustic impedance that matches that of the substrate. This allows acoustic energy to travel from
17 the substrate into the backing material (as opposed to getting reflected into the substrate at the
18 substrate-backing interface). Second, the material should be lossy. This allows for the energy
19 that enters the backing material from the substrate to be dissipated. In one preferred embodiment
20 of the invention, a tungsten epoxy mixture is used to successfully damp the longitudinal ringing
21 mode in a 640 μm silicon substrate by applying the material to the backside of the substrate (the
22 side opposite the transducer diaphragms).

24 BRIEF DESCRIPTION OF THE DRAWINGS

25 The features, objects and advantages of the present invention will become more apparent
26 from the detailed description set forth below when taken in conjunction with the drawings in
27 which like reference characters identify correspondingly throughout and wherein:

28 FIG. 1A illustrates a cross-section of one cell of a conventional capacitive
29 microfabricated transducer;

30 FIG. 1B illustrates the concept of a force on the lower electrode causing a ringing mode.

31 FIGS. 2A and 2B illustrate a cross-sectional and top view, respectively, of a capacitive
32 microfabricated transducer formed over integrated circuits;

1 FIG. 3 is a cross-sectional view of a microfabricated transducer with damping material
2 according to a preferred embodiment of the present invention;

3 FIGS. 4A-4D illustrate the experimental results obtained from applying a backing
4 material to a microfabricated ultrasonic transducer.
5

6 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

7 Reference will now be made in detail to the preferred embodiments of the invention,
8 examples of which are illustrated in the accompanying drawings. While the invention will be
9 described in conjunction with the preferred embodiments, it will be understood that they are not
10 intended to limit the invention to those embodiments. On the contrary, the invention is intended
11 to cover alternatives, modifications and equivalents, which may be included within the spirit and
12 scope of the invention as defined by the appended claims.

13 FIGS 1A and 1B illustrate a cross-section of one cell of a capacitive microfabricated
14 acoustic or ultrasonic transducer, and the concept of launching a substrate mode. A transducer
15 cell includes, among others, a diaphragm 360 with a top electrode 350, a cavity 340, a lower
16 electrode 320 on a substrate 10. When a bias and an alternating voltage are applied across
17 electrodes 320 and 350, an time-varying attractive force sets the diaphragm 360 in motion, which
18 launches an acoustic wave in the medium of interest. The force on electrode 350 is identical to
19 the force on electrode 320, however, and thus a mode can be excited in the substrate 10 such as
20 the longitudinal resonant mode depicted in FIG 1B.

21 FIGS. 2A and 2B illustrate one embodiment of a part of an array of acoustic or ultrasonic
22 transducers formed over circuit devices on the same integrated circuit. FIG. 2B illustrates a top
23 view at the top electrode level that shows the relative placement of the top electrodes 350A,
24 350B and 350C of the transducers 100A, 100B and 100C, respectively, in relation to certain
25 interconnects 230A, 230B and 230C, described further hereinafter. The cross section of Fig 2A
26 can be seen from the line A-A shown in Fig. 2B and illustrates circuit components 50 formed in
27 the semiconductor substrate 10. The circuit components 50 can form a variety of circuit
28 functions. Examples include analog circuits such as amplifiers, switches, filters, and tuning
29 networks, digital circuits such as multiplexors, counters, and buffers, and mixed signal circuits
30 (circuits containing both digital and analog functions) such as digital-to-analog and analog-to-
31 digital converters. Disposed over the circuit components 50 are transducers, such as the
32 illustrated transducers 100A, 100B and 100C. Transducers 100A, 100B and 100C are shown as

1 being composed of a single transducer cell 200A, 200B and 200C, respectively. Of course the
2 transducers 100 may have as few as one or many more than three, such as hundreds or
3 thousands, transducer cells 200 associated with them. Many such transducers 100 will typically
4 be formed at the same time on a wafer, with the wafer cut into different die as is known in the
5 art. A further description of such a transducer can be found in pending U.S. Patent Application
6 No. 09/344,312 entitled, "Microfabricated Transducers Formed Over Other Circuit Components
7 on an Integrated Circuit Chip and Methods for Making the Same," filed 6/24/99. Other
8 variations of microelectronic microfabricated immersion transducers are described in U.S. Patent
9 Application No. 09/315,896 entitled, "Acoustic transducer and method of making same," filed
10 5/20/99 by Ladabaum.

11 A preferred embodiment of the present invention will first be described with respect to
12 FIG 3. It should be noted that FIG 3 is not drawn to geometrical scale, but serves only as a
13 conceptual sketch. In FIG 3, a backing material layer 5 is disposed beneath the substrate 10.
14 This backing material, if it has a substantially similar acoustic impedance to that of substrate 10,
15 is lossy, and is of sufficient thickness to dissipate the acoustic energy in the substrate 10, will
16 suppress any ringing mode in the substrate 10. Of significance to this embodiment is the fact
17 that electronic circuit components 50 are present in the substrate 10, that the capacitive
18 transducers 100 are formed over the electronic circuit components, and that the backing layer 5 is
19 disposed beneath the substrate 10.

20 In another preferred embodiment of the present invention, substrate 10 can be made thinner
21 such that the longitudinal mode of the substrate occurs outside of the frequency band of interest,
22 either with or without the use of a backing material. For example, of significance is that the first
23 longitudinal ringing mode of a silicon substrate 640 microns thick occurs at approximately 7 MHz.
24 Thus, a preferred embodiment in which a 10 MHz center frequency diaphragm design is not
25 perturbed by substrate ringing modes is characterized by a substrate thickness of approximately 210
26 microns. At 210 microns, the first longitudinal ringing mode occurs at approximately 21 MHz, well
27 out of the 10 MHz frequency band of interest.

28 FIGS 4A-4D illustrate the experimental results of a preferred embodiment of the present
29 invention. In this embodiment, capacitive transducers operating with a center frequency of 10 MHz
30 were designed, and the transducer thus operates in the ultrasonic range. As is evident in the result of
31 a pitch-catch transmission test of two identical transducers without backing, there is a longitudinal
32 ringing mode in the 640 micron silicon substrate at approximately 7 MHz and subsequent

1 harmonics. FIG 4A is the time domain waveform of the received signal and FIG 4B is the
2 frequency domain waveform of the ratio of the transmitted to received signal. The ringing is
3 evident in the sinusoidal tail of FIG 4A and the frequency content of the ringing is evident in the
4 insertion loss plot of FIG 4B. FIGS 4C and 4D contain the results of the same transmission pitch
5 catch experiment after backing material was applied to both transducers. These figures illustrate
6 that the ringing mode has been eliminated.

7 The backing material used in this embodiment was a 20-1 weight mixture of 20 um
8 spherical tungsten powder and epoxy. This mixture was empirically derived in order to match the
9 acoustic impedance of the silicon substrate and to be very lossy. Furthermore, it forms a good bond
10 with the silicon substrate. A thickness of 1 mm of backing material was applied to the backside of
11 the silicon substrate. Of course, other lossy material can be used, particularly if matched with the
12 acoustic impedance of the substrate.

13 The present invention, as described hereinabove, thus provides for the suppression of
14 acoustic modes by placing a judiciously designed damping material on the backside of
15 electronics, something that cannot be achieved with piezoelectric transducers that require mode
16 suppression to occur directly at the piezoelectric surface. The present invention also
17 advantageously provides for thinning the substrate in order to ensure that the substrate modes are
18 outside of the frequency range of interest, which also cannot be achieved with piezoelectric
19 transducers because the dimensions of piezoelectrics define their frequency range.

20 Accordingly, while the present invention has been described herein with reference to
21 particular embodiments thereof, a latitude of modification, various changes and substitutions are
22 intended in the foregoing disclosure. For example, only certain features and not others of the
23 present invention can be used to suppress acoustic modes and still be within the intended scope
24 of the present invention. Accordingly, it will be appreciated that in some instances some
25 features of the invention will be employed without a corresponding use of other features without
26 departing from the spirit and scope of the invention.